SIPROTEC 4 7UM61 Multifunction Generator and Motor Protection Relay



Fig. 11/1 SIPROTEC 4 7UM61 multifunction generator and motor protection relay

Description

The SIPROTEC 4 7UM61 protection relays can do more than just protect. They also offer numerous additional functions. Be it earth faults, short-circuits, overloads, overvoltage, overfrequency or underfrequency, protection relays assure continued operation of power stations. The SIPROTEC 4 7UM61 protection relay is a compact unit which has been specially developed and designed for the protection of small and medium-sized generators. They integrate all the necessary protection functions and are particularly suited for the protection of:

- Hydro and pumped-storage generators
- Co-generation stations
- Private power stations using regenerative energy sources such as wind or biogases
- Diesel generator stations
- Gas-turbine power stations
- Industrial power stations
- Conventional steam power stations.

The device can also be used for protecting synchronous and asynchronous motors.

The integrated programmable logic functions (continuous function chart CFC) offer the user high flexibility so that adjustments can easily be made to the varying power station requirements, on the basis of special system conditions.

The flexible communication interfaces are open for modern communication architectures with the control system.

Function overview

Basic version

- Stator earth-fault protection
- Sensitive earth-fault protection
- Stator overload protection
- Overcurrent-time protection (either definite-time or inverse-time)
- Definite-time overcurrent-time protection, directional
- Undervoltage and overvoltage protection
- Underfrequency and overfrequency protection
- Reverse power protection
- Overexcitation protection
- External trip coupling

Standard version

Scope of basic version plus:

- Forward-power protection
- Underexcitation protection
- Negative-sequence protection
- Breaker failure protection

Full version

Scope of standard version plus:

- Inadverdent energization protection
- 100 % stator earth-fault protection with 3rd harmonic
- Impedance protection

Asynchronous motor

Scope of standard version plus

- Motor starting time supervision
- Restart inhibit (without underexcitation protection)

Monitoring functions

- Trip circuit supervision
- Fuse failure monitor
- Operational measured values V, I, f, ...
- Every metering value W_p , W_q
- Time metering of operation hours
- Self-supervision of relay
- 8 oscillographic fault records

Communication interfaces

- System interface
 - IEC 60870-5-103 protocol
 - PROFIBUS-DP
 - MODBUS RTU
 - DNP 3.0

Application

The 7UM6 protection relays of the SIPROTEC 4 family are compact multifunction units which have been developed for small to medium-sized power generation plants. They incorporate all the necessary protective functions and are especially suitable for the protection of:

- Hydro and pumped-storage generators
- Co-generation stations
- Private power stations using regenerative energy sources such as wind or biogases
- Power generation with diesel generators
- Gas turbine power stations
- Industrial power stations
- Conventional steam power stations.

They can also be employed for protection of motors and transformers.

The numerous other additional functions assist the user in ensuring cost-effective system management and reliable power supply. Measured values display current operating conditions. Stored status indications and fault recording provide assistance in fault diagnosis not only in the event of a disturbance in generator operation.

Combination of the units makes it possible to implement effective redundancy concepts.

Protection functions

Numerous protection functions are necessary for reliable protection of electrical machines. Their extent and combination are determined by a variety of factors, such as machine size, mode of operation, plant configuration, availability requirements, experience and design philosophy.

This results in multifunctionality, which is implemented in outstanding fashion by numerical technology.

In order to satisfy differing requirements, the combination of functions is scalable (see Table 11/1). Selection is facilitated by division into groups.

Protection functions	Abbre- ANSI No. viation		Generator			
			Basic	Stan- dard	Full	Motor async.
Stator earth-fault protection non-directional, directional	$V_0>$, $3I_0>$ \(V_0 , $3I_0$)	59N, 64G 67G	X	X	X	X
Sensitive earth-fault protection (also rotor earth-fault protection)	$I_{\mathrm{EE}}\!\!>$	50/51GN (64R)	X	X	X	X
Stator overload protection	I^2t	49	X	X	X	X
Definite-time overcurrent protection with undervoltage seal-in	<i>I>+V<</i>	51	X	X	X	X
Definite-time overcurrent protection, directional	<i>I>></i> , Direc.	50/51/67	X	X	X	X
Inverse-time overcurrent protection	t = f(I) + V <	51V	X	X	X	X
Overvoltage protection	V >	59	X	X	X	X
Undervoltage protection	V <	27	X	X	X	X
Frequency protection	<i>f</i> <, <i>f</i> >	81	X	X	X	X
Reverse-power protection	-P	32R	X	X	X	X
Overexcitation protection (Volt/Hertz)	V/f	24	X	X	X	
Fuse failure monitor	$V_2/V_1, I_1/I_2$	60FL	X	X	X	X
External trip coupling (7UM611/612)	Incoup.		2/4	2/4	2/4	2/4
Trip circuit supervision (7UM612)	T.C.S.	74TC	X	X	X	X
Forward-power protection	<i>P></i> , <i>P</i> <	32F		X	X	X
Underexcitation protection	1/xd	40		X	X	
Negative-sequence protection	$I_2>, t=f(I_2)$	46		X	X	X
Breaker failure protection	$I_{\min}>$	50BF		X	X	X
Inadvertent energization protection	<i>I></i> , <i>V</i> <	50/27			X	
100 %-stator-earth-fault protection with 3 rd harmonics	$V_{0(3^{\mathrm{rd}}\mathrm{harm})}$	59TN 27TN (3 rd h	.)		X	
Impedance protection with $(I >+V <)$ -pickup	<i>Z</i> <	21			X	
Motor starting time supervision	$I_{\rm an}^2 t$	48			X	X
Restart inhibit for motors	I^2t	49 Rotor			X	X
External temperature monitoring through serial interface	ϑ (Thermo-box	38	X	X	X	X
Rate-of-frequency-change protection ¹⁾	df/dt >	81R	X	X	X	X
Vector jump supervision (voltage) ¹⁾	$\Delta \varphi >$		X	X	X	X

Table 11/1 Scope of functions of the 7UM61

Generator Basic

One application is concentrated on small generators or as backup protection for larger generators. The function mix is also an effective addition to transformer differential protection with parallel-connected transformers. The functions are also suitable for system disconnection.

Generator Standard

This function mix is recommended for generator outputs exceeding 1 MVA. It is also suitable for protection of synchronous motors.

Another application is as backup protection for the larger block units.

Generator Full

Here, all protection functions are available and are recommended from generator outputs exceeding 5 MVA. Backup protection for the larger block units is also a recommended application.

Asynchronous motor

This protection function mix is recommended for motors up to 1 - 2 MW. It offers a wide frequency operating range from 11 Hz to 69 Hz. When an infeed is switched, the protection adapts to the changed voltage and frequency.

¹⁾ Available as an option (please refer to Order No., position 15).

Application

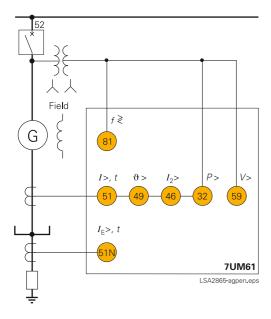


Fig. 11/2

Construction

The SIPROTEC 4 units have a uniform design and a degree of functionality which represents a whole new quality in protection and control. Local operation has been designed according to ergonomic criteria. Large, easy-to-read displays were a major design aim. The DIGSI 4 operating program considerably simplifies planning and engineering and reduces commissioning times.

The 7UM611 is configured in 1/3 19 inch, and the 7UM612 in 1/2 19 inch width. This means that the units of previous models can be replaced. The height throughout all housing width increments is 243 mm.

All wires are connected directly or by means of ring-type cable lugs.

Alternatively, versions with plug-in terminals are also available. These permit the use of prefabricated cable harnesses.

In the case of panel surface mounting, the connecting terminals are in the form of screw-type terminals at top and bottom. The communication interfaces are also arranged on the same sides.

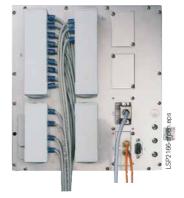


Fig. 11/3
Rear view with wiring terminal safety cover and serial interface

Definite-time overcurrent protection *I*>, *I*>> (ANSI 50, 51, 67)

This protection function comprises the short-circuit protection for the generator and also the backup protection for upstream devices such as transformers or power system protection.

An undervoltage stage at *I>* maintains the pickup when, during the fault, the current falls below the threshold. In the event of a voltage drop on the generator terminals, the static excitation system can no longer be sufficiently supplied. This is one reason for the decrease of the short-circuit current.

The *I*>> stage can be implemented as high-set instantaneous trip stage. With the integrated directional function it can be applied for generators without star point CT (see Figure 11/4).

Inverse-time overcurrent protection (ANSI 51V)

This function also comprises short-circuit and backup protection and is used for power system protection with currentdependent protection devices.

IEC and ANSI characteristics can be selected (Table 11/2).

The current function can be controlled by evaluating the generator terminal voltage.

The "controlled" version releases the sensitive set current stage.

With the "restraint" version, the pickup value of the current is lowered linearly with decreasing voltage.

The fuse failure monitor prevents unwanted operation.

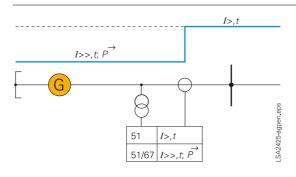


Fig. 11/4
Protection with current
transformer on terminal side

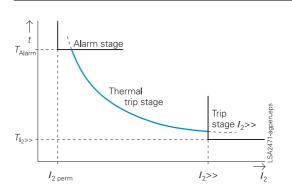


Fig. 11/5Characteristic of negative-sequence protection

Stator overload protection (ANSI 49)

The task of the overload protection is to protect the stator windings of generators and motors from high, continuous overload currents. All load variations are evaluated by the mathematical model used. The thermal effect of the r.m.s. current value forms the basis of the calculation. This conforms to IEC 60255-8. In dependency of the current the cooling time constant is automatically extended. If the ambient temperature or the temperature of the coolant are injected via PROFIBUS-DP, the model automatically adapts to the ambient conditions; otherwise a constant ambient temperature is assumed.

Negative-sequence protection (ANSI 46)

Asymmetrical current loads in the three phases of a generator cause a temperature rise in the rotor because of the negative sequence field produced.

This protection detects an asymmetrical load in three-phase generators. It functions on the basis of symmetrical components and evaluates the negative sequence of the phase currents. The thermal processes are taken into account in the algorithm and form the inverse characteristic. In addition, the negative sequence is evaluated by an independent stage (alarm and trip) which is supplemented by a time-delay element (see Figure 11/5).

Available inverse-time characteristic

Characteristics	ANSI / IEEE	IEC 60255-3
Inverse	•	•
Moderately inverse	•	
Very inverse	•	•
Extremely inverse	•	•
Definite inverse	•	

Table 11/2

Underexcitation protection (ANSI 40) (Loss-of-field protection)

Derived from the generator terminal voltage and current, the complex admittance is calculated and corresponds to the generator diagram scaled in per unit. This protection prevents damage due to loss of synchronism resulting from underexcitation. The protection function provides three characteristics for monitoring static and dynamic stability. In the event of exciter failure, fast response of the protection can be ensured via binary input. This input releases a timer with a short time delay.

The straight-line characteristics allow the protection of the generator diagram to be optimally adapted (see Fig. 11/6). The per-unit-presentation of the diagram allows the setting values to be directly read out

The positive-sequence systems of current and voltage are used to calculate the admittance. This ensures that the protection always operates correctly even with asymmetrical network conditions.

If the voltage deviates from the rated voltage, the admittance calculation has the advantage that the characteristics move in the same direction as the generator diagram.

Reverse-power protection (ANSI 32R)

The reverse-power protection monitors the direction of active power flow and picks up when the mechanical energy fails because then the drive power is taken from the network. This function can be used for operational shutdown (sequential tripping) of the generator but also prevents damage to the steam turbines. The reverse power is calculated from the positivesequence systems of current and voltage. Asymmetrical network faults therefore do not cause reduced measuring accuracy. The position of the emergency trip valve is injected as binary information and is used to switch between two trip command delays. When applied for motor protection, the sign (\pm) of the active power can be reversed via parameters.

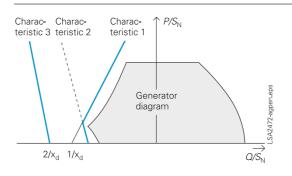


Fig. 11/6 Characteristic of underexcitation protection

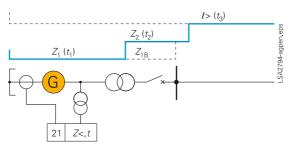


Fig. 11/7
Grading of impedance protection

Forward-power protection (ANSI 32F)

Monitoring of the active power produced by a generator can be useful for starting up and shutting down generators. One stage monitors threshold beyond one limit value while another stage monitors threshold below another limit value. The power is calculated using the positive-sequence component of current and voltage.

Impedance protection (ANSI 21)

This fast short-circuit protection protects the generator, the generator transformer and is a backup protection for the power system. This protection has two settable impedance stages; in addition, the first stage can be switched over via binary input. With the circuit-breaker in "open" position (see Fig. 11/7) the impedance measuring range can be extended. The overcurrent pickup element with undervoltage seal-in ensures a reliable pickup and the loop selection logic a reliable detection of the faulty loop. With this logic it is possible to perform a correct measurement via the unit transformer.

Undervoltage protection (ANSI 27)

The undervoltage protection evaluates the positive-sequence components of the voltages and compares them with the threshold values. There are two stages available.

The undervoltage function is used for asynchronous motors and pumped-storage stations and prevents the voltage-related instability of such machines.

The function can also be used for monitoring purposes.

Overvoltage protection (ANSI 59)

This protection prevents insulation faults that result when the voltage is too high.

Either the maximum line-to-line voltages or the phase-to-earth voltages (for low-voltage generators) can be evaluated. The measuring results of the line-to-line voltages are independent of the neutral point displacement caused by earth-faults. This function is implemented in two stages.

Frequency protection (ANSI 81)

The frequency protection prevents impermissible stress of the equipment (e.g. turbine) in case of under or overfrequency. It also serves as a monitoring and control element.

The function has four stages; the stages can be implemented either as underfrequency or overfrequency protection. Each stage can be delayed separately.

Even in the event of voltage distortion, the frequency measuring algorithm reliably identifies the fundamental waves and determines the frequency extremely precisely. Frequency measurement can be blocked by using an undervoltage stage.

Overexcitation protection Volt/Hertz (ANSI 24)

The overexcitation protection serves for detection of an unpermissible high induction (proportional to *Vlf*) in generators or transformers, which leads to thermal overloading. This may occur when starting up, shutting down under full load, with weak systems or under isolated operation. The inverse characteristic can be set via seven points derived from the manufacturer data.

In addition, a definite-time alarm stage and an instantaneous stage can be used.

For calculation of the *Vlf* ratio, frequency and also the highest of the three line-to-line voltages are used. The frequency range that can be monitored comprises 11 to 69 Hz.

Stator earth-fault protection, non-directional, directional (ANSI 59N, 64G, 67G)

Earth faults manifest themselves in generators that are operated in isolation by the occurrence of a displacement voltage. In case of unit connections, the displacement voltage is an adequate, selective criterion for protection.

For the selective earth-fault detection, the direction of the flowing earth current has to be evaluated too, if there is a direct connection between generator and busbar.

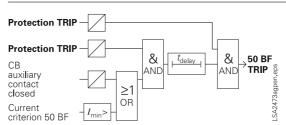


Fig. 11/8 Logic diagram of breaker failure protection

The protection relay measures the displacement voltage at a VT located at the transformer star point or at the broken delta-winding of a VT. As an option, it is also possible to calculate the zero-sequence voltage from the phase-to-earth voltages. Depending on the load resistor selection, 90 to 95 % of the stator winding of a generator can be protected.

A sensitive current input is available for earth-current measurement. This input should be connected to a core-balance current transformer. The fault direction is deduced from the displacement voltage and earth current. The directional characteristic (straight line) can be easily adapted to the system conditions. Effective protection for direct connection of a generator to a busbar can therefore be established. During start-up, it is possible to switch over from the directional to the displacement voltage measurement via an externally injected signal.

Depending on the protection setting, various earth-fault protection concepts can be implemented with this function (see Figs. 11/17 to 11/21).

Sensitive earth-fault protection (ANSI 50/51GN, 64R)

The sensitive earth-current input can also be used as separate earth-fault protection. It is of two-stage form. Secondary earth currents of 2 mA or higher can be reliably handled.

Alternatively, this input is also suitable as rotor earth-fault protection. A voltage with rated frequency (50 or 60 Hz) is connected in the rotor circuit via the interface unit 7XR61. If a higher earth current is flowing, a rotor earth fault has occurred. Measuring-circuit monitoring is provided for this application (see Figure 11/20).

100 % stator earth-fault protection with 3. harmonic (ANSI 59TN, 27TN (3H.))

Owing to the design, the generator produces a 3rd harmonic that forms a zero system. It is verifiable by the protection on a broken delta winding or on the neutral transformer. The magnitude of the voltage amplitude depends on the generator and its operation.

In the event of an earth fault in the vicinity of the neutral point, there is a voltage displacement in the 3rd harmonic (dropping in the neutral point and rising at the terminals).

Depending on the connection, the protection must be set in either undervoltage or overvoltage form. It can also be delayed. So as to avoid overfunction, the active power and the positive-sequence voltage act as enabling criteria.

The final protection setting can be made only by way of a primary test with the generator.

Breaker failure protection (ANSI 50BF)

In the event of scheduled downtimes or a fault in the generator, the generator can remain on line if the circuit-breaker is defective and could suffer substantial damage.

Breaker failure protection evaluates a minimum current and the circuit-breaker auxiliary contact. It can be started by internal protective tripping or externally via binary input. Two-channel activation avoids overfunction (see Figure 11/8).

Inadvertent energization protection (ANSI 50, 27)

This protection has the function of limiting the damage of the generator in the event of an unintentional switch-on of the circuit-breaker, whether the generator is standing still or rotating without being excited or synchronized. If the power system voltage is connected, the generator starts as an asynchronous machine with a large slip and this leads to excessively high currents in the rotor.

A logic circuit consisting of sensitive current measurement for each phase, measured value detector, time control and blocking as of a minimum voltage, leads to an instantaneous trip command. If the fuse failure monitor responds, this function is ineffective.

Starting time supervision (motor protection only) (ANSI 48)

Starting time supervision protects the motor against long unwanted start-ups, which might occur as a result of excessive load torque or excessive voltage drops within the motor, or if the rotor is locked.

The tripping time is dependent on the square of the start-up current and the set start-up time (Inverse Characteristic). It adapts itself to the start-up with reduced voltage. The tripping time is determined in accordance with the following formula:

$$t_{\text{Trip}} = \left(\frac{I_{\text{start}}}{I_{\text{rms}}}\right)^2 \cdot t_{\text{start max}}$$

 t_{Trip} Tripping time

*I*_{start} Permissible start-up current

t_{start max} Permissible start-up time

 $I_{\rm rms}$ Measured r.m.s. current value

Calculation is not started until the current $I_{\rm rms}$ is higher than an adjustable response value

(e.g. 2 I_{N, MOTOR}).

If the permissible locked-rotor time is less than the permissible start-up time (motors with a thermally critical rotor), a binary signal is set to detect a locked rotor by means of a tachometer generator. This binary signal releases the set locked-rotor time, and tripping occurs after it has elapsed.

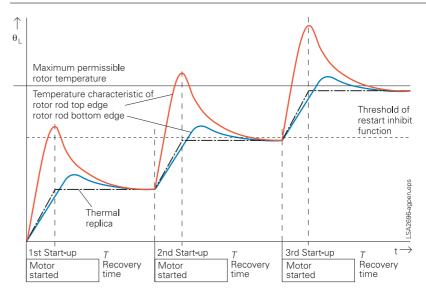


Fig. 11/9 Temperature characteristic at rotor and thermal replica of the rotor (multiple start-ups)

Restart inhibit for motors (ANSI 66, 49Rotor)

When cold or at operating temperature, motors may only be connected a certain number of times in succession. The start-up current causes heat development in the rotor which is monitored by the restart inhibit function.

Contrary to classical counting methods, in the restart inhibit function the heat and cooling phenomena in the rotor are simulated by a thermal replica. The rotor temperature is determined on the basis of the stator currents. Restart inhibit permits restart of the motor only if the rotor has enough thermal reserve for a completely new start. Fig. 11/9 illustrates the thermal profile for a permissible triple start out of the cold state. If the thermal reserve is too low, the restart inhibit function issues a blocking signal with which the motor starting circuit can be blocked. The blockage is cancelled again after cooling down and the thermal value has dropped below the pickup threshold.

As the fan provides no forced cooling when the motor is off, it cools down more slowly. Depending on the operating state, the protection function controls the cooling time constant. A value below a minimum current is an effective changeover criterion.

System disconnection

Take the case of in-plant generators feeding directly into a system. The incoming line is generally the legal entity boundary between the system owner and the in-plant generator. If the incoming line fails as the result of auto-reclosure, for instance, a voltage or frequency deviation may occur depending on the power balance at the feeding generator. Asynchronous conditions may arise in the event of connection, which may lead to damage on the generator or the gearing between the generator and the turbine. Besides the classic criteria such as voltage and frequency, the following two criteria are also applied (vector jump, rate-of-frequency-change protection).

Rate-of-frequency-change protection (ANSI 81)

The frequency difference is determined on the basis of the calculated frequency over a time interval. It corresponds to the momentary rate-of-frequency change. The function is designed so that it reacts to both positive and negative rate-of-frequency changes. Exceeding of the permissible rate-of-frequency change is monitored constantly. Release of the relevant direction depends on whether the actual frequency is above or below the rated frequency. In total, four stages are available, and can be used optionally.

Vector jump

Monitoring the phase angle in the voltage is a criterion for identifying an interrupted infeed. If the incoming line should fail, the abrupt current discontinuity leads to a phase angle jump in the voltage. This is measured by means of a delta process. The command for opening the generator or coupler circuit-breaker is issued if the set threshold is exceeded.

External trip coupling

For recording and processing of external trip information, there are 2 (for 7UM611) or 4 (for 7UM612) binary inputs. They are provided for information from the Buchholz relay or generator-specific commands and act like a protective function. Each input initiates a fault event and can be individually delayed by a timer.

Trip circuit supervision (ANSI 74TC)

One or two binary inputs can be used for monitoring the circuit-breaker trip coil including its incoming cables. An alarm signal occurs whenever the circuit is interrupted.

Phase rotation reversal

If the relay is used in a pumped-storage power plant, matching to the prevailing rotary field is possible via a binary input (generator/motor operation via phase rotation reversal).

2 pre-definable parameter groups

In the protection, the setting values can be stored in two data sets. In addition to the standard parameter group, the second group is provided for certain operating conditions (pumped-storage power stations). It can be activated via binary input, local control or DIGSI 4.

Lockout (ANSI 86)

All binary outputs (alarm or trip relays) can be stored like LEDs and reset using the LED reset key. The lockout state is also stored in the event of supply voltage failure. Reclosure can only occur after the lockout state is reset.

Fuse failure and other monitoring

The relay comprises high-performance monitoring for the hardware and software.

The measuring circuits, analog-digital conversion, power supply voltages, memories and software sequence (watch-dog) are all monitored

The fuse failure function detects failure of the measuring voltage due to short-circuit or open circuit of the wiring or VT and avoids overfunction of the undervoltage elements in the protection functions.

The positive and negative-sequence system (voltage and current) are evaluated.

Filter time

All binary inputs can be subjected to a filter time (indication suppression).

Communication

With respect to communication, particular emphasis has been placed on high levels of flexibility, data integrity and utilization of standards common in energy automation. The design of the communication modules permits interchangeability on the one hand, and on the other hand provides openness for future standards (for example, Industrial Ethernet).

Local PC interface

The PC interface accessible from the front of the unit permits quick access to all parameters and fault event data. The use of the DIGSI 4 operating program during commissioning is particularly advantageous.

Rear-mounted interfaces

Two communication modules on the rear of the unit incorporate optional equipment complements and permit retrofitting. They assure the ability to comply with the requirements of different communication interfaces (electrical or optical) and protocols (IEC 60870, PROFIBUS, DIGSI).

The interfaces make provision for the following applications:

Service interface

In the RS485 version, several protection units can be centrally operated with DIGSI 4. By using a modem, remote control is possible. This provides advantages in fault clearance, in particular in unmanned substations.

System interface

This is used to communicate with a control or protection and control system and supports, depending on the module connected, a variety of communication protocols and interface designs.

IEC 60870-5-103

IEC 60870-5-103 is an internationally standardized protocol for communication with protection relays.

IEC 60870-5-103 is supported by a number of protection unit manufacturers and is used worldwide.

The generator protection functions are stored in the manufacturer-specific, published part of the protocol.

PROFIBUS-DP

PROFIBUS is an internationally standardized communication protocol (EN 50170). PROFIBUS is supported internationally by several hundred manufacturers and has to date been used in more than 1,000,000 applications all over the world.

With the PROFIBUS-DP, the protection can be directly connected to a SIMATIC S5/S7. The transferred data are fault data, measured values and information from or to the logic (CFC).

MODBUS RTU

MODBUS is also a widely utilized communication standard and is used in numerous automation solutions.

DNP 3.0

DNP 3.0 (Distributed Network Protocol version 3) is a messaging-based communication protocol. The SIPROTEC 4 units are fully Level 1 and Level 2 compliant with DNP 3.0. DNP 3.0 is supported by a number of protection device manufacturers.

Safe bus architecture

• RS485 bus

With this data transmission via copper conductors, electromagnetic interference influences are largely eliminated by the use of twisted-pair conductor. Upon failure of a unit, the remaining system continues to operate without any faults.

• Fiber-optic double ring circuit
The fiber-optic double ring circuit is immune to electromagnetic interference.
Upon failure of a section between two units, the communication system continues to operate without disturbance.

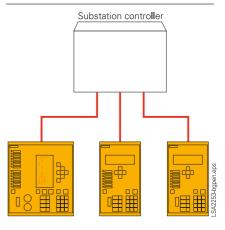


Fig. 11/10
IEC 60870-5-103 star-type RS232 copper conductor connection or fiber-optic connection

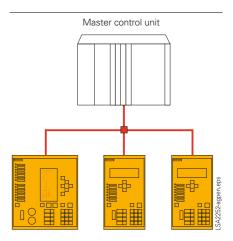


Fig. 11/11
PROFIBUS: RS485 copper conductors

Communication

System solution

SIPROTEC 4 is tailor-made for use in SIMATIC-based automation systems.

Via the PROFIBUS-DP, indications (pickup and tripping) and all relevant operational measured values are transmitted from the protection unit.

Via modem and service interface, the protection engineer has access to the protection devices at all times. This permits remote maintenance and diagnosis (cyclic testing).

Parallel to this, local communication is possible, for example, during a major inspection.







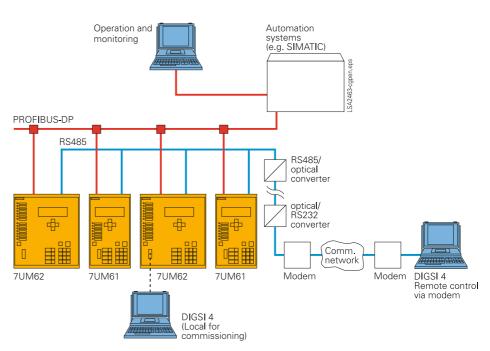


Fig. 11/15
System solution: Communication

Direct generator - busbar connection

Fig. 11/16 illustrates the recommended standard connection if several generators supply one busbar. Phase-to-earth faults are disconnected by employing the directional earth-fault criterion. The earth-fault current is driven through the cables of the system. If this is not sufficient, an earthing transformer connected to the busbar supplies the necessary current (maximum approximately 10 A) and permits a protection range of up to 90 %. The earth-fault current should be detected by means of core-balance current transformers in order to achieve the necessary sensitivity. The displacement voltage can be used as earth-fault criterion during starting operations until synchronization is achieved.

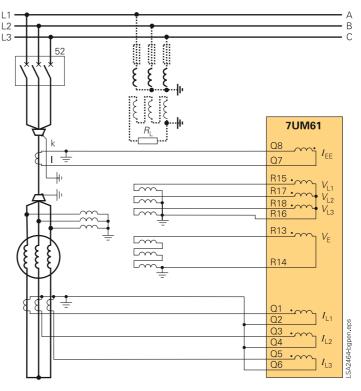


Fig. 11/16

Direct generator - busbar connection with low-resistance earthing

If the generator neutral point has low-resistance earthing, the connection illustrated in Fig. 11/17 is recommended. In the case of several generators, the resistance must be connected to only one generator, in order to prevent circulating currents (3rd harmonic).

For selective earth-fault detection, the earth-current input should be looped into the common return conductor of the two current transformer sets (differential connection). The current transformers must be earthed at only one point. The displacement voltage $V_{\rm E}$ is utilized as an additional enabling criterion.

Balanced current transformers are desirable with this form of connection. In the case of higher generator power (for example, I_N approximately 2000 A), current transformers with a secondary rated current of 5 A are recommended.

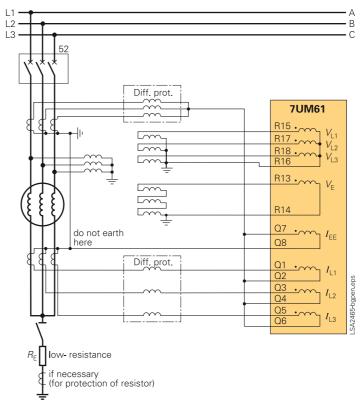


Fig. 11/17

Direct generator - busbar connection with high-resistance generator neutral earthing

With this system configuration, selective earth-fault detection is implemented on the basis of the lower fault currents through the differential connection of core-balance current transformers (see Figure 11/18). Secondary-side earthing must be effected at only one core-balance current transformer. The displacement voltage is to be utilized additionally as enable criterion.

The load resistor takes the form either of primary or of secondary resistor with neutral transformer. In the case of several generators connected to the busbar, again only one generator will be earthed via the resistor.

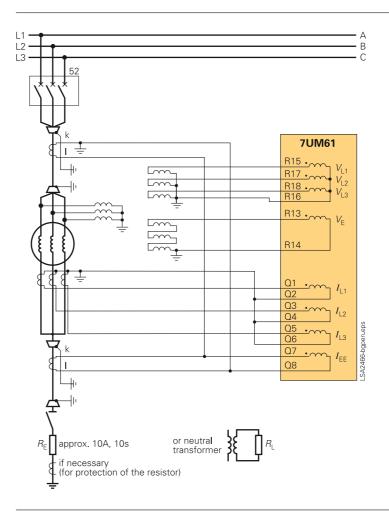


Fig. 11/18

Unit connection with isolated star point

This configuration of unit connection is a variant to be recommended (see Figure 11/19). Earth-fault detection is effected by means of the displacement voltage. In order to prevent unwanted operation in the event of earth faults in the system, a load resistor must be provided at the broken delta winding. Depending on the plant (or substation), a voltage transformer with a high power (VA) may in fact be sufficient. If not, an earthing transformer should be employed. The available measuring winding can be used for the purpose of voltage measurement.

Rotor earth-fault protection can be implemented with the unassigned earth-fault current input. The 7XR61 coupling unit must be used for this purpose.

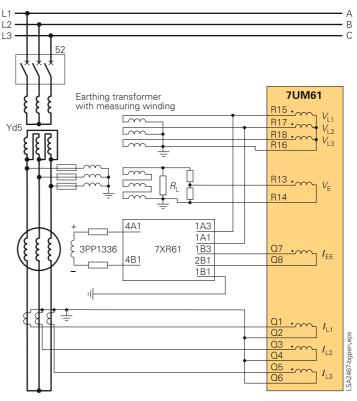


Fig. 11/19

Unit connection with neutral transformer

With this system configuration, disturbance voltage reduction and damping in the event of earth faults in the generator area are effected by a load resistor connected to generator neutral point. The maximum earth-fault current is limited to approximately 10 A. Configuration can take the form of a primary or secondary resistor with neutral transformer. In order to avoid low secondary resistance, the transformation ratio of the neutral transformer should be low. The higher secondary voltage can be reduced by means of a voltage divider.

Electrically, the circuit is identical to the configuration in Figure 11/19.

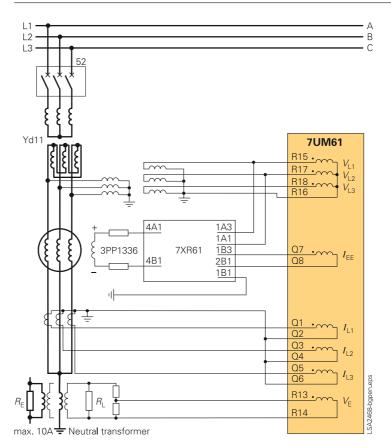


Fig. 11/20

Connection with low-voltage generators

As is generally known, the low-voltage system is solidly earthed, so that the generator neutral point is connected to earth (see Figure 11/21). With this configuration, there is the risk that, as a result of the 3rd harmonics forming a zero phase-sequence system, circulating currents will flow via the N-conductor. This must be limited by the generator or system configuration (reactor).

Otherwise, connection corresponds to the customary standard. In the case of residual current transformer design, it has to be ensured that the thermal current limit (1 s) of the I_{EE} input is restricted to 300 A.

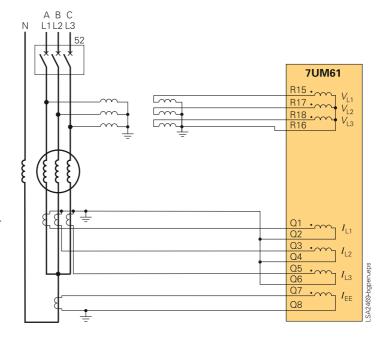


Fig. 11/21

Connection of an asynchronous motor

The figure shows the standard connection of motors of medium capacity (500 kW to <(1-2) MW). In addition to the short-circuit protection, an earth-fault protection (V_E ; I_E inputs) is available.

As the busbar voltage is being monitored, starting of the motor is prevented if the voltage is too low or - in case of failure of infeed - the motor circuit-breaker is opened. Here, the wide range of frequency is advantangeous. For the detection of temperatures, 2 thermo-boxes (temperature monitoring boxes) can be connected via a serial interface.

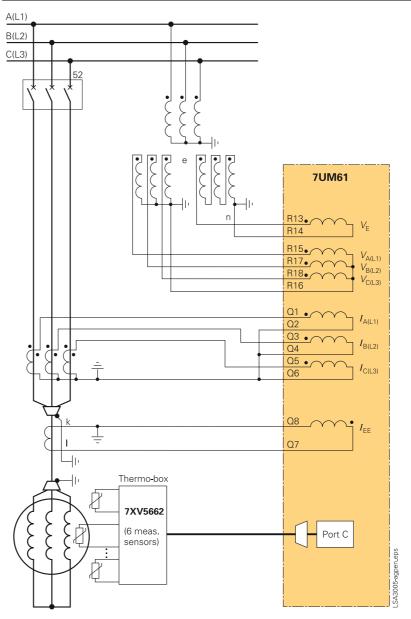


Fig. 11/22

Voltage transformer in open delta connection (V-connection)

Protection can also be implemented on voltage transformers in open delta connection. Figure 11/23 shows the connection involved. If necessary, the operational measured values for the phase-to-earth voltages can be slightly asymmetrical. If this is disturbing, the neutral point (R16) can be connected to earth via a capacitor.

In the case of open delta connection, it is not possible to calculate the displacement voltage from the secondary voltages. It must be passed to the protection relay along a different path (for example, voltage transformer at the generator neutral point or from the earthing transformer).

Connection with two current transformers

This configuration is to be found in older systems with insulated or high-resistance star point. This connection is illustrated in Fig. 11/24. In the protection unit, the secondary currents are represented correctly and, in addition, the positive and the negative-sequence system are correctly calculated. Limits of application occur in the case of low-resistance and solid earthing.

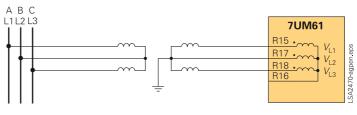


Fig. 11/23

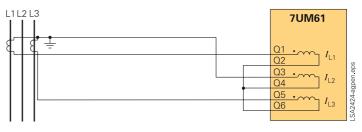


Fig. 11/24

Technical data

50 or 60 Hz
1 or 5 A
1.6 A
100 to 125 V
Approx. 0.05 VA Approx. 0.3 VA Approx. 0.05 VA Approx. 0.3 VA
100 I_N for 1 s 30 I_N for 10 s 4 I_N continuous
250 I _N (one half cycle)
300 A for 1 s 100 A for 10 s 15 A continuous 750 A (one half cycle)
230 V continuous
24 to 48 V DC 60 to 125 V DC 110 to 250 V DC and 115 V/230 V AC with 50/60 Hz
-20 to +20 %
≤ 15 %
Approx. 4 W Approx. 4.5 W Approx. 9.5 W Approx. 12.5 W
≥ 50 ms ≥ 20 ms
7 15 10 to 19 V DC or 44 to 88 V DC 88 to 176 V DC ¹⁾ 300 V DC Approx. 1.8 mA

Output relays	
Number 7UM611 7UM612	12 (1 NO, 1 optional as NC, via jumper) 20 (1 NO, 2 optional as NC,
Switching capacity Make Break Break (for resistive load) Break (for L/R ≤ 50 ms) Switching voltage Permissible current	via jumper) 1000 W / VA 30 VA 40 W 25 VA 250 V 5 A continuous 30 A for 0.5 seconds
LEDs	
Number RUN (green) ERROR (red) Assignable LED (red) 7UM611	1 1 7
7UM612	14
Unit design	p. l' ' l' '
7XP20 housing Degree of protection acc. to EN 60529 For surface-mounting housing For flush-mounting housing Front Rear For the terminals Weight Flush mounting housing 7UM611 (1/3 x 19") 7UM612 (1/2 x 19") Surface mounting housing 7UM611 (1/3 x 19") 7UM612 (1/2 x 19")	For dimensions see dimension drawings, part 15 IP 51 IP 51 IP 50 IP 2x with terminal cover put on Approx. 5.5 kg Approx. 7 kg Approx. 12 kg

Technical data Ε Serial interfaces S Operating interface for DIGSI 4 Connection Non-isolated, RS232, front panel; S 9-pin subminiature connector Baud rate 4800 to 115200 baud Time synchronization IRIG-B / DCF 77 signal (Format IRIG-B000) Connection 9-pin subminiature connector, Ir terminal with surface-mounting housing Voltage levels Selectable 5 V or 12 V or 24 V Service/modem interface for DIGSI 4/modem/service p Isolated RS232/RS485 9-pin subminiature connector Test voltage 500 V / 50 Hz Distance for RS232 Max. 15 m Max. 1000 m Distance for RS485 Fiber-optic cable Integrated ST-connector R Optical wavelength $\lambda = 820 \text{ nm}$ Permissible path attenuation Max. 8 dB for glass-fiber 62.5/125 μm Bridgeable distance Max. 1.5 km System interface IEC 60870-5-103 protocol, PROFIBUS-DP, MODBUS RTU ti Isolated RS232/RS485 9-pin subminiature connector E Baud rate 4800 to 115200 baud Test voltage 500 V / 50 Hz Distance for RS232 Max. 15 m Distance for RS485 Max. 1000 m PROFIBUS RS485 Test voltage 500 V / 50 Hz Max. 12 Mbaud Baud rate Distance 1000 m at 93.75 kBaud; 100 m at 12 Mbaud PROFIBUS fiber-optic Only for flush-mounting housing ST connector Optical interface with OLM1) For surface-mounting housing Baud rate Max. 1.5 Mbaud Optical wavelength $\lambda = 820 \text{ nm}$ Permissible path attenuation Max. 8 dB for glass-fiber 62.5/125 μm Distance 1.6 km (500 kB/s) 530 m (1500 kB/s) IEC 60255-22-4, IEC 61000-4-4, class IV 1) Conversion with external OLM

Electrical tests	
Specifications	
Standards	IEC 60255 (product standards) ANSI/IEEE C37.90.0/.1/.2 UL 508 DIN 57435, part 303 For further standards see below.
nsulation tests	
Standards	IEC 60255-5
Voltage test (100 % test) All circuits except for auxiliary sup- ply, binary inputs communication and time synchronization interfaces	2.5 kV (r.m.s.), 50/60 Hz
Voltage test (100 % test) Auxiliary voltage and binary inputs	3.5 kV DC
Voltage test (100 % test) RS485/RS232 rear side communica- tion interfaces and time synchroni- teation interface	500 V (r.m.s. value), 50/60 Hz
Impulse voltage test (type test) All circuits except for communica- tion interfaces and time synchroni- teation interface, class III	5 kV (peak); 1.2/50 μs ; 0.5 J; 3 positive and 3 negative impulses at intervals of 5 s
EMC tests for noise immunity; type tes	it
Standards	IEC 60255-6, IEC 60255-22 (product standards) EN 50082-2 (generic standard) DIN 57435 part 303
High fraguancy toot	2.5 kV (pook volue) 1 MHz.

S High frequency test 2.5 kV (peak value), 1 MHz; IEC 60255-22-1, class III $\tau = 15$ ms, 400 pulses per s; and VDE 0435 part 303, class III duration 2 s Electrostatic discharge 8 kV contact discharge; 15 kV air IEC 60255-22-2, class IV discharge; both polarities; EN 61000-4-2, class IV 150 pF; R_i = 330 Ω Irradiation with RF field, 10 V/m; 27 to 500 MHz non-modulated IEC 60255-22-3 (report), class III Irradiation with RF field, 10 V/m; 80 to 1000 MHz; 80 % AM; amplitude-modulated 1 kHz IEC 61000-4-3, class III

Irradiation with RF field,
pulse-modulated, IEC 61000-4-3/
ENV 50204, class III

Fast transient interference bursts

10 V/m; 900 MHz; repetition frequency 200 Hz; duty cycle 50 %

4 kV; 5/50 ns; 5 kHz; burst length

4 kV; 5/50 hs; 5 kHz; burst length = 15 ms; repetition rate 300 ms; both polarities; $R_i = 50 \Omega$; test duration 1 min

For fiber-optic interface please complete order number at 11th position with 4 (FMS RS485) or 9 and Order code LOA (DP RS485) and additionally order:

For single ring: SIEMENS OLM 6GK1502-3AB10 For double ring: SIEMENS OLM 6GK1502-4AB10

Technical data

EMC tests for noise immunity; type te	sts	Mechanical stress tests		
High-energy surge voltages			ismic vibration	
(SURGE), IEC 61000-4-5 Installation, class III	·	During operation		
Auxiliary supply	Common (longitudinal) mode:	Standards	IEC 60255-21 and IEC 60068	
,,	2 kV; 12 Ω , 9 μF Differential (transversal) mode: 1 kV; 2 Ω , 18 μF	Vibration IEC 60255-21-1, class 2 IEC 60068-2-6	Sinusoidal 10 to 60 Hz; ± 0.075 mm ampli- tude;	
Measurement inputs, binary inputs and relay outputs	Common (longitudinal) mode: 2 kV ; 42Ω , $0.5 \mu\text{F}$ Differential (transversal) mode:		60 to 150 Hz: 1 g acceleration Frequency sweep 1 octave/min 20 cycles in 3 orthogonal axes	
Line-conducted HF, amplitude- modulated IEC 61000-4-6, class III	$1~kV;42~\Omega,0.5~\mu F$ $10~V;150~kHz$ to $80~MHz;$ $80~\%~AM;1~kHz$	Shock IEC 60255-21-2, class 1 IEC 60068-2-27	Half-sinusoidal Acceleration 5 g, duration 11 ms, 3 shocks each in both directions of the 3 axes	
Magnetic field with power frequency IEC 61000-4-8, class IV; IEC 60255-6	30 A/m continuous; 300 A/m for 3 s; 50 Hz 0.5 mT; 50 Hz	Seismic vibration IEC 60255-21-2, class 1 IEC 60068-3-3	Sinusoidal 1 to 8 Hz: ± 3.5 mm amplitude (horizontal axis) 1 to 8 Hz: ± 1.5 mm amplitude	
Oscillatory surge withstand capability ANSI/IEEE C37.90.1	2.5 to 3 kV (peak); 1 to 1.5 MHz damped wave; 50 surges per second; Duration 2 s; $R_i = 150$ to 200 Ω		(vertical axis) 8 to 35 Hz: 1 g acceleration (horizontal axis) 8 to 35 Hz: 0.5 g acceleration	
Fast transient surge withstand capability ANSI/IEEE C37.90.1	4 to 5 kV; 10/150 ns; 50 surges per second; both polarities; Duration 2 s; $R_i = 80 \Omega$		(vertical axis) Frequency sweep 1 octave/min 1 cycle in 3 orthogonal axes	
Radiated electromagnetic interfer-	35 V/m; 25 to 1000 MHz	During transport	, ,	
ence ANSI/IEEE C37.90.2		Standards	IEC 60255-21 and IEC 60068-2	
Damped oscillations IEC 60894, IEC 61000-4-12	2.5 kV (peak value), polarity alternating 100 kHz, 1 MHz, 10 and 50 MHz, $R_{\rm i} = 200~\Omega$	Vibration IEC 60255-21-1, class 2 IEC 60068-2-6	Sinusoidal 5 to 8 Hz: ±7.5 mm amplitude; 8 to 150 Hz: 2 g acceleration Frequency sweep 1 octave/min	
EMC tests for interference emission;			20 cycles in 3 orthogonal axes	
Standard Conducted interference voltage on lines only auxiliary supply IEC-CISPR 22	EN 50081-1 (generic standard) 150 kHz to 30 MHz Limit class B	Shock IEC 60255-21-2, class 1 IEC 60068-2-27	Half-sinusoidal Acceleration 15 g, duration 11 ms, 3 shocks each in both directions 3 axes	
Interference field strength IEC-CISPR 22	30 to 1000 MHz Limit class B	Continuous shock IEC 60255-21-2, class 1 IEC 60068-2-29	Half-sinusoidal Acceleration 10 g, duration 16 ms, 1000 shocks in both directions of the 3 axes	

Technical data

Climatic stress tests	
Temperatures	
Type-tested acc. to IEC 60068-2-1 and -2, test Bd, for 16 h	–25 °C to +85 °C / –13 °F to +185 °F
Temporarily permissible operating temperature, tested for 96 h	–20 °C to +70 °C / –4 °F to +158 °F
Recommended permanent operating temperature acc. to IEC 60255-6	-5 °C to +55 °C / +25 °F to +131 °F
 Limiting temperature during permanent storage Limiting temperature during transport 	-25 °C to +55 °C / −13 °F to +131 °F -25 °C to +70 °C / −13 °F to +158 °F
Humidity	
Permissible humidity stress It is recommended to arrange the units in such a way that they are not exposed to direct sunlight or pronounced temperature changes that could cause condensation	Annual average ≤ 75 % relative humidity; on 56 days a year up to 93 % relative humidity; condensation is not permitted

could cause condensation	
Functions	
General	
Frequency range	11 to 69 Hz
Definite-time overcurrent protection,	directional (ANSI 50, 51, 67)
Setting ranges Overcurrent $I>$, $I>>$ Time delay T Undervoltage seal-in $V<$ Seal-in time of $V<$ Angle of the directional element (at $I>$) Times	0.1 to 8 A (steps 0.01 A); 5 times at $I_N = 5$ A 0 to 60 s (steps 0.01 s) or indefinite 10 to 125 V (steps 0.1 V) 0.1 to 60 s (steps 0.01 s) -90 ° to $+90$ ° (steps 1 °)
Pickup time <i>I</i> >, <i>I</i> >> At 2 times of set value At 10 times of set value Drop-off time <i>I</i> >, <i>I</i> >> Drop-off ratio Drop-off ratio <i>V</i> <	Approx. 35 ms Approx. 25 ms Approx. 50 ms <i>I</i> >: 0.95; <i>I</i> >>: 0.9 to 0.99 (steps 0.01) Approx. 1.05
Tolerances Current pickup (starting) I>, I>> Undervoltage seal-in V< Angle of the directional element Time delays	1 % of set value or 10/50 mA 1 % of set value or 0.5 V 1 ° 1 % or 10 ms

Inverse-time overcurrent protection (ANSI 51V) Setting ranges 0.1 to 4 A (steps 0.01 A); 5 times at $I_{\rm N} = 5$ A Pickup overcurrent I_P 0.05 to 3.2 s (steps 0.01 s) Time multiplier IEC-characteristics T or indefinite Time multiplier 0.5 to 15 (steps 0.01) or indefinite ANSI-characteristics DUndervoltage release V<10 to 125 V (steps 0.1 V) Trip characteristics IEC Normal inverse; very inverse; extremely inverse ANSI Inverse; moderately inverse; very inverse; extremely inverse; definite inverse Pickup threshold Approx. 1.1 IP Drop-off threshold Approx. 1.05 I_P for $I_P/I_N \ge 0.3$ Tolerances Pickup threshold $I_{\rm P}$ $1\ \%$ of set value 10/50 mA Pickup threshold *V*< $1\ \%$ of set value or 0.5 V Time for $2 \le I/I_P \le 20$ 5 % of nominal value + 1 % current

tolerance or 40 ms

Stator overload protection, thermal (ANSI 49)

Stator overload protection, the	ermal (ANSI 49)
Setting ranges	
Factor k according to	0.5 to 2.5 (steps 0.01)
IEC 60255-8	
Time constant	30 to 32000 s (steps 1 s)
Time delay factor at standst	
Alarm overtemperature	70 to 100 % related to the trip
$\Theta_{ m Alarm}/\Theta_{ m Trip}$	temperature (steps 1 %)
Overcurrent alarm stage I_{Ala}	, 1
	$I_{\rm N}=5~{ m A}$
Temperature at $I_{\rm N}$	40 to 200 °C (steps 1 °C)
	or 104 to 392 °F (steps 1 °F)
Scaling temperature of cooli	. 1
medium	or 104 to 572 °F (steps 1 °F)
Reset time at emergency star	20 to 150000 s (steps 1 s)
Drop-off ratio	
$\Theta/\Theta_{\mathrm{Trip}}$	Drop-off with Θ_{Alarm}
$\Theta/\Theta_{ m Alarm}$	Approx. 0.99
I/I _{Alarm}	Approx. 0.95
Tolerances	
Regarding k x I_P	2 % or 10/50 mA; class 2 %
	according to IEC 60255-8
Regarding trip time	3 % or 1 s: class 3 %
0 0 1	according to IEC 60255-8
	for $I/(k I_N) > 1.25$

Technical data				
Negative-sequence protection (ANSI	46)		Forward-power protection (ANSI 32F))
Setting ranges Permissible negative sequence I_2 perm. I_N Definite time trip stage $I_2 >>/I_N$ Time delays T_{Alarm} ; $T_{12}>>$ Negative-sequence factor k Cooling down time $T_{Cooling}$	10 to 100 0 to 60 s (2 to 40 s ((steps 1 %) % (steps 1 %) steps 0.01 s) or indefinite steps 0.1 s) o s (steps 1 s)	Setting ranges Forward power $P_{Forw.} < /S_N$ Forward power $P_{Forw.} > /S_N$ Time delays T Times Pickup time	0.5 to 120 % (steps 0.1 %) 1 to 120 % (steps 0.1 %) 0 to 60 s (steps 0.01 s) or indefinite Approx. 360 ms (50 Hz);
Times Pickup time (definite stage) Drop-off time (definite stage) Drop-off ratios I_2 perm.; $I_2 >>$	Approx. 5 Approx. 5 Approx. 0	0 ms 0 ms	(accurate measuring) Pickup time (fast measuring) Drop-off time (accurate measuring)	Approx. 300 ms (60 Hz) Approx. 60 ms (50 Hz); Approx. 50 ms (60 Hz) Approx. 360 ms (50 Hz); Approx. 300 ms (60 Hz)
Drop-off ratio thermal stage Tolerances	Drop-off	at fall below of I_2 perm.	Drop-off time (fast measuring)	Approx. 60 ms (50 Hz); Approx. 50 ms (60 Hz)
Pickup values I_2 perm.; $I_2 >>$ Time delays	3 % of set sequence 1 % or 10	value or 0.3 % negative	Drop-off ratio $P_{Forw.}$ Drop-off ratio $P_{Forw.}$ Tolerances	1.1 or 0.5 % of S _N Approx. 0.9 or –0.5 % of S _N
Thermal characteristic Time for $2 \le I_2/I_2$ perm. ≤ 20		minal value +1 % current	Active power $P_{\text{Forw.}} <$, $P_{\text{Forw.}} >$	0.25 % $S_N \pm 3$ % of set value at $Q < 0.5$ S_N at accurate measuring
Underexcitation protection (ANSI 40)				$0.5 \% S_N \pm 3 \%$ of set value at $Q < 0.5 S_N$ at fast measuring
Setting ranges Conductance thresholds 1/xd	0.25 to 2.6) (-1 0.01)	Time delays T	1 % or 10 ms
characteristic (3 characteristics)		(steps 0.01)	Impedance protection (ANSI 21)	
Inclination angle α_1 , α_2 , α_3 Time delay T		° (steps 1°) steps 0.01 s) or indefinite	Setting ranges Overcurrent pickup <i>I</i> >	0.1 to 4 A (steps 0.01 A); 5 times at $I_N = 5A$
Times Stator criterion $1/xd$ characteristic; α	Approx. 6		Undervoltage seal-in V < Impedance Z1 (related to $I_N = 1$ A)	10 to 125 V (steps 0.1V) 0.05 to 130 Ω (steps 0.01 Ω)
Undervoltage blocking Drop-off ratio Stator criterion $1/xd$ characteristic; α Undervoltage blocking	Approx. 0 Approx. 1	.95	Impedance Z1B (related to $I_N = 1$ A) Impedance Z2 (related to $I_N = 1$ A) Time delays T	0.05 to $65~\Omega$ (steps $0.01~\Omega$) 0.05 to $65~\Omega$ (steps $0.01~\Omega$) 0 to $60~s$ (steps $0.01~s$) or indefinite
Tolerances Stator criterion $1/xd$ characteristic Stator criterion α Undervoltage blocking Time delays T	3 % of set 1 ° electric 1 % or 0.5 1 % or 10	value cal 5 V	Times Shortest tripping time Drop-off time Drop-off ratio Overcurrent pickup <i>I</i> >	Approx. 40 ms Approx. 50 ms
Reverse-power protection (ANSI 32R)			Undervoltage seal-in V<	Approx. 1.05
Setting ranges Reverse power $P_{\text{Rev.}} > /S_{\text{N}}$ Time delays T		30 % (steps 0.01 %) steps 0.01 s) or indefinite	Tolerances Overcurrent pickup I > Undervoltage seal-in V < Impedance measuring Z1, Z2 Time delays T	1 % of set value. 10/50 mA 1 % of set value. or 0.5 V $ \Delta Z/Z \le 5$ % for 30 ° $\le \varphi_K \le 90$ ° 1 % or 10 ms
Pickup time		60 ms (50 Hz);	Undervoltage protection (ANSI 27)	
Drop-off time	Approx. 3	00 ms (60 Hz) 60 ms (50 Hz); 00 ms (60 Hz)	Setting range Undervoltage pickup V<, V<< (positive sequence as phase-to-phase values)	10 to 125 V (steps 0.1 V)
Tolerances Reverse power $P_{\text{Rev.}}$ > Time delays T	0.25 % S _N 1 % or 10	± 3 % set value	Time delays T Times Pickup time $V <$, $V <<$	0 to 60 s (steps 0.01 s) or indefinite Approx. 50 ms
,			Drop-off time $V <$, $V < <$	Approx. 50 ms
			Drop-off ratio $V <$, $V <$	1.01 to 1.1 (steps 0.01)
				1 % of set value or 0.5 V 1 % or 10 ms

Technical data			
Overvoltage protection (ANSI 59)		90 % stator earth-fault protection, r (ANSI 59N, 64G, 67G)	on-directional, directional
Setting ranges Overvoltage pickup V>, V>> (maximum phase-to-phase voltage or phase-to-earth-voltage) Time delays T	30 to 170 V (steps 0.1 V) 0 to 60 s (steps 0.01 s) or indefinite	Setting ranges Displacement voltage $V_0 >$ Earth current $3I_0 >$ Angle of direction element Time delays T	5 to 125 V (steps 0.1 V) 2 to 1000 mA (steps 1 mA) 0 to 360 ° (steps 1 °) 0 to 60 s (steps 0,01 s) or indefinite
Time	o to oo o (steps olor o) or machine	Times	o to oo o (steps 0,01 b) of machine
Pickup times $V>$, $V>>$ Drop-off times $V>$, $V>>$	Approx. 50 ms Approx. 50 ms	Pickup times V_0 >, $3I_0$ > Drop-off times V_0 >/ $3I_0$ >	Approx. 50 ms Approx. 50 ms
Drop-off ratio <i>V</i> >, <i>V</i> >>	0.9 to 0.99 (steps 0.01)	Drop-off ratio V_0 >, $3I_0$ > Drop-off difference angle	0.7 10 ° directed to power system
Tolerances Voltage limit value Time delays T	1 % of set value 0.5 V 1 % or 10 ms	Tolerances Displacement voltage	1 % of set value or 0.5 V
Frequency protection (ANSI 81)		Earth current Time delays <i>T</i>	1 % of set value or 0.5 mA 1 % or 10 ms
Setting ranges	4	Sensitive earth-fault protection (ANS	
Steps; selectable <i>f></i> , <i>f</i> < Pickup values <i>f></i> , <i>f</i> < Time delays <i>T</i> Undervoltage blocking <i>V</i> ₁ <	4 40 to 65 Hz (steps 0.01 Hz) 0 to 60 s (steps 0.01 s) or indefinite 10 to 125 V (steps 0.1 V)	Setting ranges Earth current pickup I_{EE} >, I_{FE} >>	2 to 1000 mA (steps 1 mA)
Times Pickup times <i>f</i> >, <i>f</i> < Drop-off times <i>f</i> >, <i>f</i> <	Approx. 100 ms Approx. 100 ms	Time delays T Measuring circuit supervision $I_{\rm EE}<$	0 to 60 s (steps 0.01 s) or indefinite 1.5 to 50 mA (steps 0.1 mA)
Drop-off difference Δf Drop-off ratio $V_1 <$	Approx. 20 mHz Approx. 1.05	Times Pickup times Drop-off times	Approx. 50 ms Approx. 50 ms
Tolerances Frequency Undervoltage blocking Time delays <i>T</i>	10 mHz (at <i>V</i> > 0.5 <i>V</i> _N) 1 % of set value or 0.5 V 1 % or 10 ms	Measuring circuit supervision Drop-off ratio I_{EE} >, I_{EE} >> Drop-off ratio measuring circuit	Approx. 50 ms 0.95 or 1 mA Approx. 1.1 or 1 mA
Overexcitation protection (Volt/Hert	z) (ANSI 24)	supervision $I_{\rm EE}<$ Tolerances	
Setting ranges Pickup threshold alarm stage Pickup threshold V/f>>-stage	1 to 1.2 (steps 0.01) 1 to 1.4 (steps 0.01)	Earth current pickup Time delays T	1 % of set value or 0.5 mA 1 % or 10 ms
Time delays <i>T</i> Characteristic values of <i>V/f</i>	0 to 60 s (steps 0.01 s) or indefinite 1.1/1.15/1.2/1.25/1.3/1.35/1.4	100 % stator earth-fault protection (ANSI 59TN, 27TN (3 H.))	with 3 harmonics
and assigned times $t(V/f)$ Cooling down time $T_{Cooling}$	0 to 20000 s (steps 1 s) 0 to 20000 s (steps 1 s)	Setting ranges Displacement voltage V_0 (3 rd harm.) >, V_0 (3 rd harm.) <	0.2 to 40 V (steps 0.1 V)
Times (Alarm and <i>V/f>>-stage</i>) Pickup times at 1.1 of set value Drop-off times	Approx. 60 ms Approx. 60 ms	Time delay <i>T</i> Active-power release Positive-sequence voltage release	0 to 60 s (steps 0.01 s) or indefinite 10 to 100 % (steps 1 %) or indefinite 50 to 125 V (steps 0.1 V) or indefinite
Drop-off ratio (alarm, trip)	0.95	Times	50 to 125 v (steps 0.1 v) of indefinite
Tolerances V/f-pickup	3 % of set value	Pickup time Drop-off time	Approx. 80 ms Approx. 80 ms
Time delays <i>T</i> Thermal characteristic (time)	1 % or 10 ms 5 % rated to <i>Vlf</i> or 600 ms	Drop-off ratio Undervoltage stage $V_{0 \text{ (3}^{\text{rd}} \text{ harm.})} <$ Overvoltage stage $V_{0 \text{ (3}^{\text{rd}} \text{ harm.})} >$ Active-power release Positive-sequence voltage release	Approx. 1.4 Approx. 0.6 Approx. 0.9 Approx. 0.95
		Tolerances Displacement voltage Time delay T	3 % of set value or 0.1 V 1 % or 10 ms

Technical data				
Breaker failure protection (ANSI 50BF)		Restart inhibit for motors (ANSI 66, 49 Rotor)		
Setting ranges Current thresholds <i>I</i> >BF Time delay BF- <i>T</i>	0.04 to 1 A (steps 0.01 A) 0.06 to 60 s (steps 0.01 s) or indefinite	Setting ranges Motor starting current I _{Start max} /I _N Permissible starting	3.0 to 10.0 (steps 0.01) 3.0 to 120.0 s (steps 0.1 s)	
Time Pickup time Drop-off time	Approx. 50 ms Approx. 50 ms	time $T_{\text{Start max}}$ Rotor temperature equalization time $T_{\text{Equali.}}$ Minimum restart inhibit	0 to 60.0 min (steps 0,1 min) 0.2 to 120.0 min (steps 0.1 min)	
Tolerances Current threshold $I>BF/I_N$ Time delay T	1 % of set value or 10/50 mA 1 % or 10 ms	time $T_{ m Restart, min}$ Permissible number of warm starts $n_{ m W}$	1 to 4	
Inadvertent energizing protection (A	ANSI 50, 27)	Difference between warm and cold starts n _K -n _W	1 to 2	
Setting ranges Current pickup $I>>>$ Voltage release $V_1<$	0.1 to 20 A (steps 0.1 A); 5 times at I_N = 5 A 10 to 125 V (steps 1 V)	Extensions of time constants (running and stop) Tolerances	1.0 to 100.0	
Time delay	0 to 60 s (steps 0.01 s) or indefinite	Time delays T	1 % or 0.1 ms	
Drop-off time	0 to 60 s (steps 0.01 s) or indefinite	Rate-of-frequency-change protection	n (ANSI 81R)	
Times Reaction time Drop-off time Drop-off ratio $I>>>$ Drop-off ratio $V_1<$	Approx. 25 ms Approx. 35 ms Approx. 0.8 Approx. 1.05	Setting ranges Steps, selectable +df/dt >; - df/dt Pickup value df/dt Time delays T Undervoltage blocking V_1 <	4 0.2 to 10 Hz/s (steps 0.1 Hz/s); 0 to 60 s (steps 0.01 s) or indefinite 10 to 125 V (steps 0.1 V)	
Tolerances Current pickup Undervoltage seal-in V_1 < Time delay T	5 % of set value or 20/100 mA 1 % of set value or 0.5 V 1 % or 10 ms	Times Pickup times df/dt Drop-off times df/dt Drop-off ratio df/dt	Approx. 200 ms Approx. 200 ms Approx. 0.95 or 0.1 Hz/s	
External trip coupling		Drop-off ratio V<	Approx. 1.05	
Number of external trip couplings	2 for 7UM611 4 for 7UM612	Tolerances Rate-of-frequency change Undervoltage blocking	Approx. 0.1 Hz/s at V > 0.5 $V_{\rm N}$ 1 % of set value or 0.5 V	
Trip circuit supervision (ANSI 74TC)	,	Time delays T	1 % or 10 ms	
Number of supervised trip circuits (only 7UM612)	1	Vector jump supervision (voltage)		
Starting time supervision for motors	(ANSI 48)	Setting ranges Stage $\Delta \varphi$	0.5 ° to 15 ° (steps 0.1 °)	
Setting ranges Motor starting current I _{Start max} /I _N Starting current pickup I _{Start, pickup.} /I _N	1.0 to 16 (steps 0.01) 0.6 to 10 (steps 0.01)	Time delay T Undervoltage blocking V_1 < Tolerances Vector jump	0 to 60 s (steps 0.01 s) or indefinite 10 to 125 V (steps 0.1 V) $0.3\ ^{\circ}\ at\ V{>}\ 0.5\ V_{N}$	
Permissible starting	1.0 to 180 s (steps 0.1 s)	Undervoltage blocking Time delay <i>T</i>	1 % of set value or 0.5 V 1 % or 10 ms	
time $T_{\text{Start max}}$ Permissible locked rotor	0.5 to 120 s (steps 0.1 s) or indefinite	Incoupling of temperature via serial i	interface (thermo-box) (ANSI 38)	
time $T_{ m Blocking}$		Number of measuring sensors	6 or 12	
Times	Depending on the settings	Temperature thresholds	40 to 250 °C or 100 to 480 °F	
Drop-off ratio	Approx. 0.95		(steps 1 °C or 1 °F)	
Tolerances Current threshold Time delays <i>T</i>	1 % of set value, or 1 % of $I_{\rm N}$ 5 % or 30 ms	Sensor types	Pt100; Ni 100, Ni 120	

Technical data

Technical data			
Operational measured values			
Description	Primary; secondary or per unit (%)		
Currents Tolerance	$I_{\rm L1};I_{\rm L2};I_{\rm L3};I_{\rm EE};I_1;I_2$ 0.2 % of measured values or \pm 10 mA \pm 1 digit		
Voltages	$V_{L1}; V_{L2}; V_{L3}; V_E; V_{L12}; V_{L23}; V_{L31}; V_1; V_2$		
Tolerance	0.2 % of measured values or \pm 0.2 V \pm 1 digit		
Impedance Tolerance	R, X 1 %		
Power Tolerance	S; P; Q 1 % of measured values or \pm 0.25 % S_N		
Phase angle Tolerance	φ <0.1 °		
Power factor Tolerance	$\cos \varphi$ (p.f.) 1 % ± 1 digit		
Frequency Tolerance	f 10 mHz at ($V\!\!>$ 0.5 $V_{\rm N};$ 40 Hz $<$ f $<$ 65 Hz)		
Overexcitation Tolerance	V/f; 1 %		
Thermal measurement Tolerance	$\begin{array}{l}\Theta_{L1};\Theta_{L2},\Theta_{L3},\Theta_{12},\Theta_{V/f},\\5~\%\end{array}$		
Min./max. memory			
Memory	Measured values with date and time		
Reset manual	Via binary input Via key pad Via communication		
Values Positive sequence voltage Positive sequence current Active power Reactive power Frequency Displacement voltage (3 rd harmonics)	V_1 I_1 P Q f $V_{E(3}^{rd}$ harm.)		
Energy metering			
Meter of 4 quadrants Tolerance	W _{P+} ; W _{P-} ; W _{Q+} ; W _{Q-} 1 %		
Fault records			
Number of fault records	Max. 8 fault records		
Instantaneous values Storage time Sampling interval	Max. 5 s Depending on the actual frequency (e. g. 1.25 ms at 50 Hz; 1.04 ms at 60 Hz))		
Channels	$v_{\text{L1}}, v_{\text{L2}}, v_{\text{L3}}, v_{\text{E}}; i_{\text{L1}}, i_{\text{L2}}, i_{\text{L3}}, i_{\text{EE}}$		
R.m.s. values Storage period Sampling interval Channels	Max. 80 s Fixed (20 ms at 50 Hz; 16.67 ms at 60 Hz)		
Salancio	$V_1,V_{ ext{E}},I_1,I_2,I_{ ext{EE}},P,Q,arphi,f_{ ext{fn}}$		

Additional functions	
Fault event logging	Storage of events of the last 8 faults Puffer length max. 600 indications Time solution 1 ms
Operational indications	Max. 200 indications Time solution 1 ms
Elapsed-hour meter	Up to 6 decimal digits (criterion: current threshold)
Switching statistics	Number of breaker operation Phase-summated tripping current

CE conformity

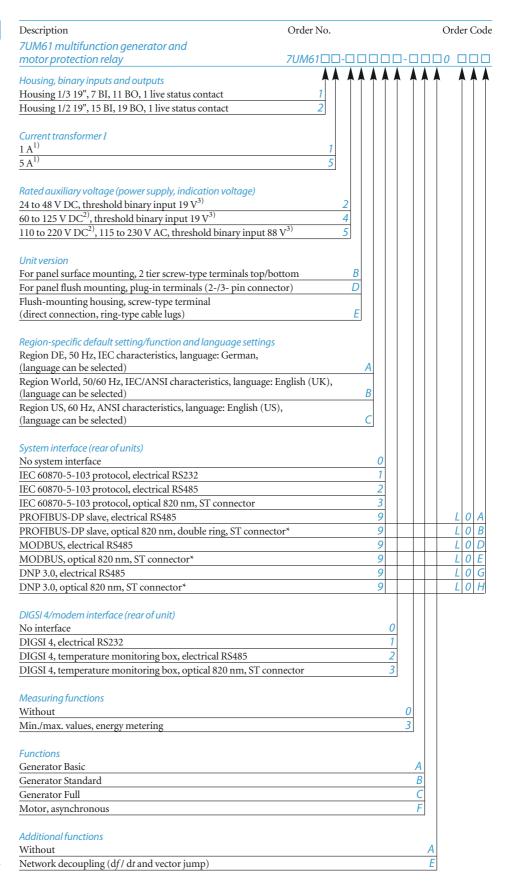
This product is in conformity with the Directives of the European Communities on the harmonization of the laws of the Member States relating to electromagnetic compatibility (EMC Council Directive 89/336/EEC) and electrical equipment designed for use within certain voltage limits (Council Directive 73/23/EEC).

This unit conforms to the international standard IEC 60255, and the German standard DIN 57435/Part 303 (corresponding to VDE 0435/Part 303).

The unit has been developed and manufactured for application in an industrial environment according to the EMC standards.

This conformity is the result of a test that was performed by Siemens AG in accordance with Article 10 of the Council Directive complying with the generic standards EN 50081-2 and EN 50082-2 for the EMC Directive and standard EN 60255-6 for the "low-voltage Directive".

Selection and ordering data



- 1) Rated current can be selected by means of jumpers.
- Transition between the two auxiliary voltage ranges can be selected by means of jumpers.
- 3) The binary input thresholds can be selected in stages by means of jumpers.
- 4) For more detailed information on the functions see Table 11/1 on page 11/4.
- * Not with position 9 = 8; if 9 = "B", please order 7UM61 unit with RS485 port and separate fiber-optic converters.

Description	Order No.
DIGSI 4	
Software for configuration and operation of Siemens protection units	
running under MS Windows 2000/XP Profesional Edition	
device templates, Comtrade Viewer, electronic manual included	
as well as "Getting started" manual on paper, connecting cables (copper)	
Basis	
Full version with license for 10 computers, on CD-ROM	
(authorization by serial number)	7XS5400-0AA00
Professional	
DIGSI 4 Basis and additionally SIGRA (fault record analysis),	
CFC Editor (logic editor), Display Editor (editor for default	
and control displays) and DIGSI 4 Remote (remote operation)	7XS5402-0AA00
SIGRA 4	
(generally contained in DIGSI Professional, but can be ordered additionally)	
Software for graphic visualization, analysis and evaluation of fault records. Can also be used for fault records of devices of other manufacturers	
(Comtrade format). Running under MS Windows 2000/XP Professional Edition. Incl. templates, electronic manual with license for 10 PCs.	
Authorization by serial number. On CD-ROM.	7XS5410-0AA00
Authorization by serial number. On CD-ROW.	7X33410-0AA00
Connecting cable	
Cable between PC/notebook (9-pin connector)	
and protection unit (9-pin connector)	
(contained in DIGSI 4, but can be ordered additionally)	7XV5100-4
Coupling device for rotor earth-fault protection	7XR6100-0CA00
	Short code
Series resistor for rotor earth-fault protection (group: 013002)	3PP1336-0DZ K2Y
Resistor for stator earth-fault protection (voltage divider, 5: 1) (group 013001)	3PP1336-1CZ K2Y
Temperature monitoring box (thermo-box)	
24 to 60 V AC/DC	7XV5662-2AD10
90 to 240 V AC/DC	7XV5662-5AD10
M	
Manual for 7UM61	CE2000 C117C C127 2
English	C53000-G1176-C127-2

Accessories

Acces	sories
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	3-afpen.
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Fig. 11/25 Mounting rail for 19" rack



Fig. 11/26 2-pin connector

Fig. 11/27 3-pin connector



Fig. 11/28 Short-circuit link for current terminals

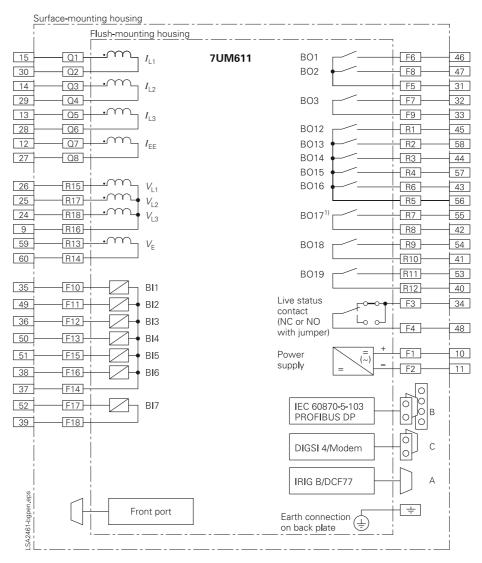


Fig. 11/29 Short-circuit link for voltage terminals/indications terminals

Description			Order No.	Size of package	Supplier	Fig.
Connector	2-pin		C73334-A1-C35-1	1	Siemens	11/26
	3-pin		C73334-A1-C36-1	1	Siemens	11/27
Crimp	CI2 0.5 to	1 mm ²	0-827039-1	4000	AMP 1)	
connector			0-827396-1	1	AMP 1)	
	CI2 1 to 2.	.5 mm²	0-827040-1	4000	AMP 1)	
	012 1 10 2	012 1 to 2.5 mm	0-827397-1	1	AMP 1)	
	Type III+	0.75 to 1.5 mm ²	0-163083-7	4000	AMP 1)	
	71		0-163084-2	1	AMP 1)	
Crimping	For Type l	III+	0-539635-1	1	AMP 1)	
tool	, .	ning female	0-539668-2		AMP 1)	
	For CI2		0-734372-1	1	AMP 1)	
	and matching female		1-734387-1		AMP 1)	
Mounting rail		C73165-A63-D200-1	1	Siemens	11/25	
Short-circuit links For current		urrent terminals	C73334-A1-C33-1	1	Siemens	11/28
	For o	ther terminals	C73334-A1-C34-1	1	Siemens	11/29
Safety cover for terminals Large Small		C73334-A1-C31-1	1	Siemens	11/3	
		C	C73334-A1-C32-1	1	Siemens	11/3

¹⁾ Your local Siemens representative can inform you on local suppliers.

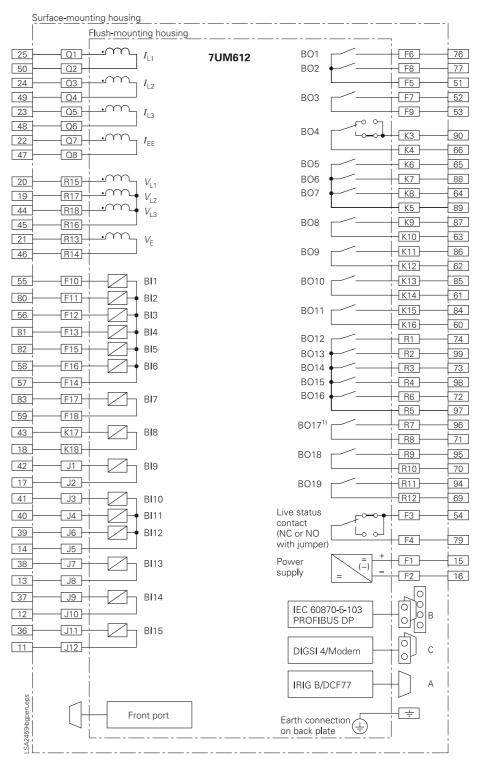
Connection diagram, IEC



1) NO or NC with jumper possible.

Fig. 11/30 7UM611 connection diagram (IEC standard)

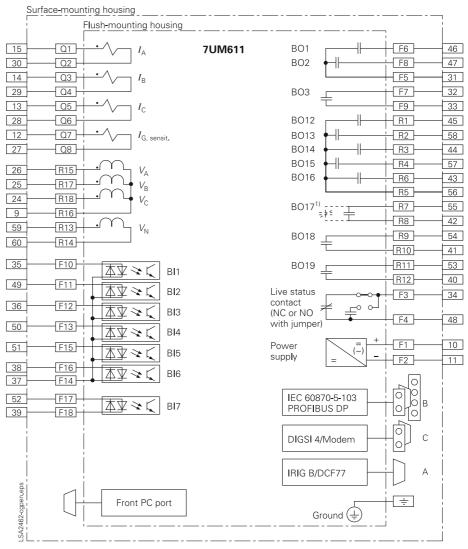
Connection diagram, IEC



1) NO or NC with jumper possible.

Fig. 11/31 7UM612 connection diagram (IEC standard)

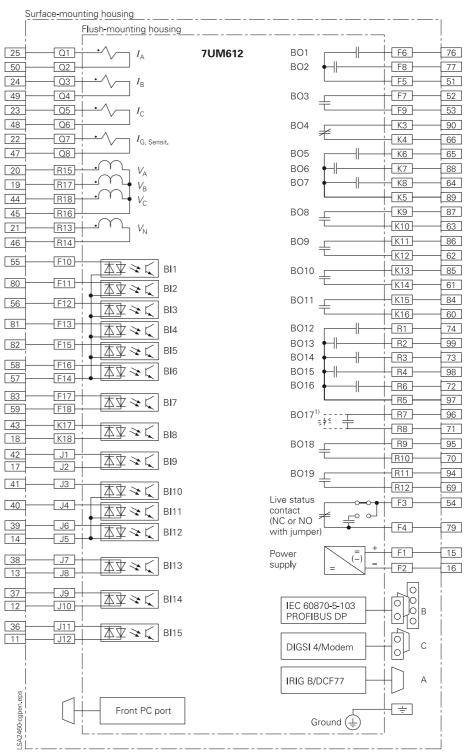
Connection diagram, ANSI



1) NO or NC with jumper possible.

Fig. 11/32 7UM611 connection diagram (ANSI standard)

Connection diagram, ANSI



1) NO or NC with jumper possible.

Fig. 11/33 7UM612 connection diagram (ANSI standard)